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A METHOD FOR LOWERING THE LEVEL OF THE ELECTROMAGNETIC WAVES BACKGROUND RADIATION OF HORN RADIATOR

The problem about decrease in horn radiator electromagnetic waves return radiation level by a method of excitation of the slowed down surface waves on an exterior side of its aperture edge, being in an antiphase with return radiation electromagnetic waves has been solved.

For practical application of this method, a pyramidal H-sector horn radiator with curvilinear walls is taken. In the construction of this method, an impedance metal comb is used, which acts as a delay line for electromagnetic waves reflected from the aperture of the radiator.

Introduction

Horn radiators (HR) refer to an aperture class of the antenna working in a range of ultrahigh frequencies (UHF). Thanks to simplicity of a design and high technical characteristics HR have found wide application in modern radio-electronic communication systems, radar-locations, tele-radio broadcasting, and also in space flying vehicle.

One of HR advantages is the high radiation orientation which is characterised by the orientation diagramme (OD). HR have wide range of working frequencies, high efficiency and possibility to radiate electromagnetic waves of the big capacity (up to 100 MW) that make them irreplaceable in a radar-location and a space radio communication.

However, there are the various factors worsening HR characteristics. In particular:

- 1) sphericity of the phase front form in a plane of HR outlet aperture;
- 2) dispersion of the radiation basic harmonic field energy inside the HR on the set of mode of the higher harmonics;
- 3) occurrence of the electromagnetic field energy return reflexion in feeding wave guide;
- 4) occurrence of return radiation into the region of space which is behind the HR.

The last is caused by a line of the phenomena in which number the most ponderable is the electromagnetic waves reradiation by the currents

induced in the HR aperture outlet edge contour (aperture).

The researches [1-9] directed on improvement of HR characteristics have led to occurrence of HR new class with curvilinear walls in which influence of the listed phenomena is considerably reduced. However, the problem of the return radiation remains actual.

In our work the new method of the return radiation level arising on an edge of HR aperture outlet reduction which is applied to pyramidal HR with curvilinear walls is offered.

1. Problem statement

Let's consider cross-section of an aperture outlet of pyramidal HR, representing the electric contour of rectangular section K_1 radiating electromagnetic waves (fig. 1). Sources of an electromagnetic field are alternating currents i_1, i_2, i_3, i_4 . Assume that each site of a contour radiates in space cylindrical waves with a length λ_0 and phase φ_0 . Let's by condention, B - the area of direct radiation located in front of HR aperture. The plane of these areas section coincides with a plane of contour K_1 . Let's place the geometrical centre of K_1 contour at the beginning of the co-

ordinate system. On an axis z in the region of semispace $A(-z, \pm x, \pm y)$ we will place contour K_2 identical to contour K_1 with the geometrical centre with coordinates $(0,0,-l)$.

Then the electromagnetic waves radiated by contour K_1 having passed distance l during t_{lag} will induce alternating currents i'_1, i'_2, i'_3, i'_4 in contour K_2 . As the result the system of two radiating contours - active K_1 and passive K_2 will turn out, and the phase of radiation of a contour $K_2 - \varphi_2$ will lag behind phase φ_0 for time necessary for an electromagnetic wave for overcoming the distance l .

At axes z in a distant zone we will pick up the point $M_{z \gg \lambda_0}$. The distance from zero of coordinate system to point $M_{z \gg \lambda_0}$ should be 10 times more the wave length λ_0 .

The electromagnetic waves radiated by contours K_1 and K_2 will reach point $M_{z \gg \lambda_0}$ not

simultaneously, and during $t_0 = \frac{R_1}{c}$ on radius-

vector R_1 and $t_{lag} = \frac{l}{v} + \frac{R_2}{c}$, where v and c -

electromagnetic waves speed of distribution between contours K_1 and K_2 , and in free space accordingly. As R_1 and R_2 is more than distance between contours l it is possible to consider, that

$$R_1 = R_2 = R.$$

It is necessary to define such time of delay t_{lag} at which in a point of supervision $M_{z \gg \lambda_0}$ phases φ_0 and φ_2 will differ from each other on size π .

$$t_{lag} - t_0 = \pi \quad (1)$$

or

$$\frac{l}{v} - \frac{l}{c} = \frac{\lambda_0}{2c} \quad (2)$$

In this case the electric and magnetic field vectors radiated by contours K_1 and K_2 are in anti-phase for any $x, y, -z$ 10 times larger than λ_0 and the resultant capacity stream density in a distant zone of semispace A tends to zero. In semispace $B(z, \pm x, \pm y)$ in a distant zone phases φ_0 and φ_2 will coincide, as the wave passes between contours the distance equal $2l$ (there and back) for corresponding time $2t_{lag} = 2\pi$.

2. Decision technique

To fulfill conditions (1-2) it is necessary to reduce the electromagnetic energy distribution speed in the region $z(0, -l)$. For this purpose we will place between conductors of contours K_1 and K_2 the slowing down comb type structure made in the form of a flat metal comb (fig. 2).

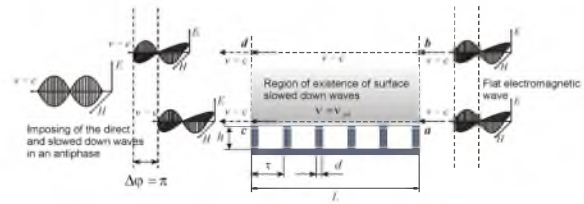


Fig. 2. A fragment of slowing down comb structure on the basis of an impedance metal comb. τ - the comb period, l - comb length, d - comb thickness, h - comb height, v - slowing down wave speed, v_{ph} - phase speed

The first comb (a) corresponds to contour K_1 , the last comb (c) corresponds to contour K_2 .

At interaction of a flat electromagnetic wave with an impedance metal comb over its surface the slowed down surface waves appear. Electrodynamics of the given process is studied enough [10-12]. Having solved the equation (2) concerning speed of the surface slowed down wave v we will receive:

$$v = c \frac{l}{\frac{\lambda_0}{2} + l} \quad (3)$$

Knowing the ν size it is possible to find all geometrical parameters of slowing down structure, namely: τ - the comb period, l - the comb length, d - the comb thickness, h - the comb height at which the condition of formula (1) will be satisfied. Using received in [2, 10, 12] expressions for slowing down inductive type structure on the basis of an impedance metal comb we will write down the common decision of a problem uniting in geometrical and electrodynamic parameters.

$$\sqrt{1 + \left(\frac{\tau - d}{\tau} \operatorname{tg} \frac{2\pi h_{\text{eff}}}{\lambda_0} \right)^2} = \frac{lc}{\frac{\lambda_0}{2} + l};$$

$$\begin{cases} l = 6 \div 8 \lambda_0; \\ \tau < 0,5 \lambda_0; \\ d \ll \tau; \\ 0 < h_{\text{eff}} < \frac{\lambda_{\text{max}}}{4}. \end{cases} \quad (4)$$

where c - speed of electromagnetic waves distribution in vacuum;

λ_0 - length of a wave corresponding to the middle of the operating band;

λ_{max} - maximum length of a wave of the operating band;

λ_{min} - minimum length of a wave of the operating band;

τ - comb period;

d - comb thickness;

l - comb length;

h_{eff} - combs effective height counted under the formula:

$$h_{\text{eff}} = h - 0.14(d + \tau),$$

where h - the constructive (in fact) edge height.

3. Results and discussion

For practical application described above method it is taken pyramidal N-sectorial HR with curvilinear walls, in which design the impedance metal comb is included (fig. 3).

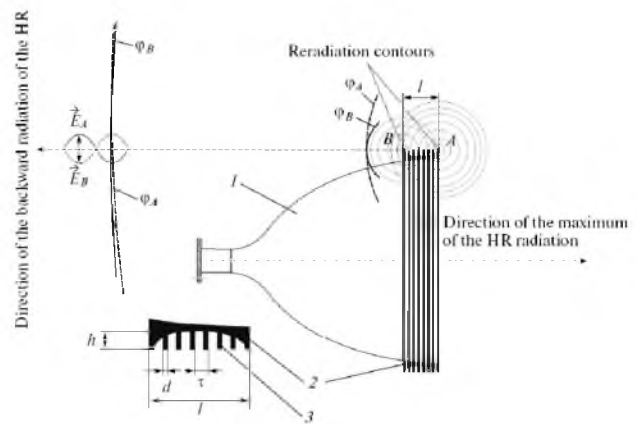


Fig. 3. H-sectorial HR with curvilinear walls of combined form with the return radiation lowered level. 1-H-sectorial HR with curvilinear walls of combined forms, 2- comb type slowing down structure in the form of a flat metal impedance comb in section, 3 - metal comb edge, l - metal comb length, τ - the comb-period, d - comb thickness, h - comb height

The prototype sample of offered HR with following parameters is made and tested:

- the minimum wavelength of the operating

band $\lambda_{\text{min}} = 24$ mm;

- the maximum wavelength of operating band

$\lambda_{\text{max}} = 36$ mm;

- the length of a horizontal rib of HR outlet

aperture $A_p = 100$ mm;

- the rib constructive height $h = 3$ mm;

- the edge thickness $d = 0,5$ mm;

- the comb period $\tau = 5$ mm;

- the comb length $l = 210$ mm;

- Metal comb flutes depth changes on exponential law.

In polar system of coordinates are constructed normalized directional diagrams (DD) of HR prototype sample (solid line) and similar HR, but without impedance comb (dotted line) (fig. 4).

4. Conclusions

The analysis of received DD allows to conclude.

1. Level of back lobe DD of HR prototype sample with an impedance comb is considerably less, than at HR without an impedance comb;

2. At observation angle of $\theta = 90^0$ concerning the radiation maximum in developed HR intensity of an electromagnetic field decreases, and at HR without an impedance comb, on the contrary, in the given point growth of intensity of an electromagnetic field is observed. Theoretical calculations and experimental researches of HR sample confirm efficiency of the offered decision.

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Key words: Horn radiator, horn antenna, surface electromagnetic waves, impedance retardation structure, radiation pattern

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МЕТОД СНИЖЕНИЯ УРОВНЯ ОБРАТНОГО ИЗЛУЧЕНИЯ ЭЛЕКТРОМАГНИТНЫХ ВОЛН РУПОРНОГО ИЗЛУЧАТЕЛЯ

Аннотация

Решена задача о снижении уровня обратного излучения электромагнитных волн рупорного излучателя методом возбуждения замедленных поверхностных волн на внешней стороне кромки его раскрыва, находящихся в противофазе с электромагнитными волнами обратного излучения.

Для практического применения данного метода взят пирамидальный Н-секториальный рупорный излучатель с криволинейными стенками, в конструкцию которого включена импедансная металлическая гребенка, выполняющая роль линии задержки для отраженных от апертуры излучателя электромагнитных волн.

Ключевые слова: Рупорный излучатель, рупорная антенна, поверхностные электромагнитные волны, импедансная замедляющая структура, диаграмма направленности.

А. О. Карпенко

МЕТОД ЗНИЖЕННЯ РІВНЯ ЗВОТНОГО ВИПРОМІНЮВАННЯ РАДІОХВИЛЬ РУПОРНОГО ВИПРОМІНЮВАЧА

Анотація

Розв'язана задача про зниження рівня зворотного випромінювання електромагнітних хвиль рупорного випромінювача шляхом збудження уповільнених поверхневих хвиль на зовнішній стороні кромки його розкриву, що знаходяться в протифазі з електромагнітними хвилями зворотного випромінювання.

Для практичного застосування даного методу взято пірамідальний Н-секторіальний рупорний випромінювач з криволінійними стінками, в конструкцію якого включена імпедансна металева гребінка, що виконує роль лінії затримки для відбитих від апертури випромінювача електромагнітних хвиль.

Ключові слова: Рупорний випромінювач, рупорна антена, поверхневі електромагнітні хвилі, імпедансна уповільнююча структура, діаграма направленості.