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ENERGY EFFICIENCY DETERMINATION OF LOADING-BACK SYSTEM OF ELECTRIC TRACTION MACHINES

Purpose. Acceptance post-repair tests of electric traction machines are conducted on loading-back stands that reduce the overall power costs for the tests. Currently a number of possible circuit designs of loading-back systems of electric machines are known, but there is no method of determining their energy efficiency. This in turn makes difficult the choice of rational options. The purpose of the article is the development of the corresponding methodology to make easier this process. **Methodology.** Expressions for determining the energy efficiency of a stand for testing of electric traction machines were obtained using the generalized scheme analysis of energy transformations in the loading-back systems of universal structure. **Findings.** The technique was offered and the analytical expressions for determining the energy efficiency of loading-back systems of electric traction machines were obtained. Energy efficiency coefficient of loading-back system is proposed to consider as the ratio of the total action energy of the mechanical and electromotive forces, providing anchors rotation and flow of currents in electric machines, which are being tested, to the total energy, consumed during the test from the external network. **Originality.** The concept was introduced and the analytical determination method of the energy efficiency of loading-back system in electric traction machines was offered. It differs by efficiency availability of power sources and converters, as well as energy efficiency factors of indirect methods of loss compensation. **Practical value.** The proposed technique of energy efficiency estimation of a loading-back system can be used in solving the problem of rational options choice of schematics stands decisions for electric traction machines acceptance tests of main line and industrial transport.

Keywords: electric traction machines; tests; loading-back; power losses; energy efficiency

Introduction

Requirements of the relevant standards and regulations for repair of locomotives provide for acceptance testing of each newly manufactured electric traction machine or machine after repair [3]. These tests are an important and integral part of technical process of production or repair of electric traction machine, the material costs for which are included in the cost of final product [10].

Technical quality control, which is conducted during the acceptance tests of electric traction machines, ultimately determines the reliability and dependability of the hauling plant as a whole and,

consequently, the cost-effectiveness of railway transportations of mainline and industrial vehicles.

The loading-back systems (where the energy exchange between the tested machines takes place) provide high energy efficiency of the tests with relatively low total power of power supply sources. External power sources in such loading-back systems are needed only to cover the power losses in the tested electric machines [4].

Reduction of power consumption for acceptance post-repair tests of electric traction machines is one of the urgent problems on repair enterprises of traction rolling stock of mainline and industrial

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vehicles. Thermal tests of electric traction machines on the test bench of loading-back are the most energy-intensive part of the entire test program. Energy consumption for this type of tests can be reduced both by increasing the energy efficiency of the loading-back system and by optimizing the mode of loading of electric traction machines [11, 13, 12].

Purpose

The purpose of this research is to develop the methods for determining the energy efficiency of loading-back systems of electric traction machines.

Methodology

The term energy efficiency is generally understood as the rational use of energy resources during some technological process.

The most known index of energy efficiency of a device performing useful work is its efficiency coefficient. That is the ratio of this useful work to the energy consumption from the network.

Despite the fact that the loading-back system does not perform useful work, the fact of the load current flow of electric machines and rotation of their anchors is the purpose of loading-back process, namely, providing the tests of electric machines tests under loading [9].

Thus, the energy efficiency of the loading-back system can be considered as the ratio of the total energy of mechanical and electromotive forces providing anchors rotation and the flow of currents in tested electric machines to the total energy consumed during the test from the external network.

In general, the energy efficiency coefficient of loading-back system can be represented as

$$k_{\text{эфс}} = \frac{A_{\text{пол}}}{A_{\text{затр}}},$$

where $A_{\text{пол}}$ и $A_{\text{затр}}$ are the useful and consumed energy accordingly.

Consumed energy $A_{\text{затр}}$ does not require detailed explanation, but, nevertheless, one should note that it will be considered as the total amount of electricity consumed during the test of electric traction machines by all the sources of system from the three-phase AC network.

The issue of what should be considered as a useful energy consumed for the test requires de-

tailed observation. If the purpose of loading-back is to ensure the load current flow and anchors (rotors) rotation, the useful power is the total power of all kinds of losses in the tested electric machines. Covering all the power losses in electric machines is the main purpose of energy sources in the system of loading-back [8]. From this point of view, the useful power of sources of loading-back system is

$$P_{\text{пол}} = \sum \Delta P_{\text{др}},$$

where $\sum \Delta P_{\text{др}}$ is the total power losses in the tested electric machines (engine and generator).

Then the energy efficiency coefficient of the loading-back system is

$$k_{\text{эфс}} = \frac{\int_0^{t_1} \sum \Delta P_{\text{др}} dt}{\int_0^{t_1} P dt},$$

where $\sum P$ – the total power consumed by the loading-back system from the network; t_1 – is the testing time.

Total power consumption $\sum P$ is consumed to cover the total power losses in the tested electric machines $\sum \Delta P_{\text{др}}$ and the total losses in regulators and converters $\sum \Delta P_{\text{пр}}$

$$\sum P = \sum \Delta P_{\text{др}} + \sum \Delta P_{\text{пр}}.$$

The energy efficiency of the loading-back system, as it was shown above, is the ratio of the total power losses in the tested electric traction machines meeting the parameters of adopted loading mode to the total power consumed by the power supply sources of loading-back system from the network. The nature of dependence of this indicator on the structure of the loading-back system can be determined by the universal scheme of energy transformations shown in Fig. 1.

This scheme is universal and takes into account all the possible options to cover the power losses in the tested electric machines [9]:

- direct covering of electric losses;
- indirect covering of electric losses;
- direct covering of idling losses;
- indirect covering of idling losses.

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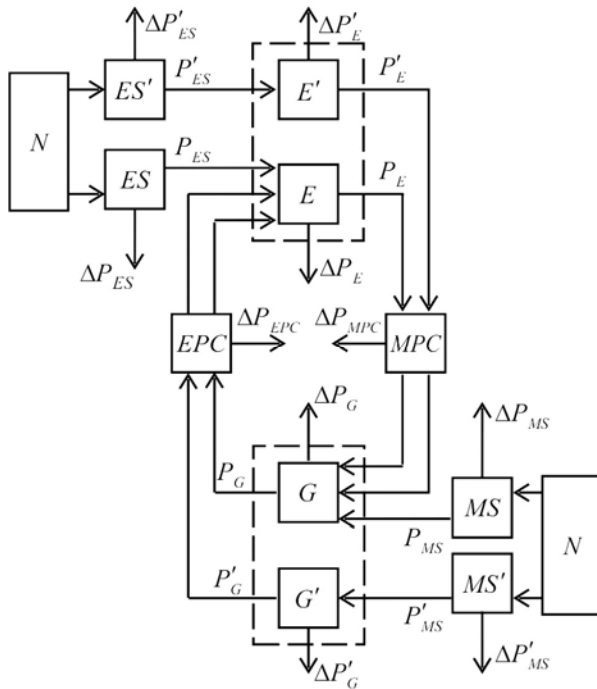


Fig. 1. Universal scheme of energy transformations in the loading-back system of electric traction machines

The scheme provides the variants of electrical and mechanical power transmission in the main power conversion loop using converters of electric and mechanical power, respectively.

Electric power source ES compensates electric losses in loading-back system by direct process, when the electric power source ES' compensates idling losses by indirect way. The source of mechanical power MS covers idling losses in the system directly, when the source of mechanical power MS' covers electrical losses indirectly. All four possible power sources are connected to the network «N».

The tested engine is conventionally divided into two parts: \mathcal{D} and \mathcal{D}' . A conditional part \mathcal{D} is included into the main loop of power transformations, and the part \mathcal{D}' is a conditional converter of ES' source electric power into mechanical power transmitted to generator G [5]. The tested generator is also conditionally divided into two parts: G and G'. Conditional part G is included into the main loop of power transformations, when the part G' is a conditional converter of MS' source mechanical power into electric power transmitted to the engine E.

Transmission of power $P_{\text{иэ}}$ of ES source to the engine E is carried out directly, when the transmission of power $P'_{\text{иэ}}$ of the ES' source to generator G is carried out through the engine E' and mechanical

power converter and the MPC. Transmission of mechanical power $P_{\mathcal{D}}$ from the tested engine E to the tested generator G is carried out through the MPC converter; when transmission of the electric power $P_{\mathcal{Г}}$ from the tested generator G to the engine E is carried out through the EPC converter.

Energy transformation loop, including the conditional part of engine E, conditional part of generator G, and the converters MPC and EPC is the main one. Total losses in the tested engine and generator caused by transformations in this loop, represent a useful power of the loading-back system.

$$\sum \Delta P_{\text{др}} = \Delta P_{\mathcal{D}} + \Delta P_{\mathcal{Г}}.$$

Total power, consumed by loading-back system from the network,

$$\sum P = P_1 + P_2 + P_3 + P_4,$$

where P_1, P_2, P_3, P_4 are the powers, consumed from the network by the sources ES, ES', MS, MS' accordingly.

In accordance with the energy transformation scheme shown in Fig. 1, the power balance can be represented as

$$\begin{aligned} \sum P = & \sum \Delta P_{\text{др}} + \Delta P_{\text{иэ}} + \Delta P'_{\text{иэ}} + \Delta P_{\text{им}} + \\ & + \Delta P'_{\text{им}} + \Delta P_{\text{прм}} + \Delta P_{\text{прэ}} + \Delta P'_{\mathcal{D}} + \Delta P'_{\mathcal{Г}}, \end{aligned}$$

where $\Delta P_{\text{иэ}}, \Delta P'_{\text{иэ}}, \Delta P_{\text{им}}, \Delta P'_{\text{им}}$ are the power losses in the sources ES, ES', MS, MS' accordingly; $\Delta P_{\text{прм}}, \Delta P_{\text{прэ}}$ are the losses in converters of mechanical and electric power accordingly; $\Delta P'_{\mathcal{D}}, \Delta P'_{\mathcal{Г}}$ are the additional power losses in the tested engine and generator accordingly.

Findings

Coefficient of energy efficiency of loading-back system can be represented as

$$k_{\text{эфс}} = \frac{\sum \Delta P_{\text{др}}}{\sum \Delta P_{\text{др}} + \sum \Delta P_{\text{пр}}},$$

where

$$\begin{aligned} \sum \Delta P_{\text{пр}} = & \Delta P_{\text{иэ}} + \Delta P'_{\text{иэ}} + \Delta P_{\text{им}} + \\ & + \Delta P'_{\text{им}} + \Delta P_{\text{прм}} + \Delta P_{\text{прэ}} + \Delta P'_{\mathcal{D}} + \Delta P'_{\mathcal{Г}}. \end{aligned}$$

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Power losses in the sources and converters are determined by their efficiency and net power at the output required for the operation of loading-back system in the set mode [7].

Note that the diagram in Fig. 1 is universal and takes into account all possible energy transformations in the loading-back system. For a particular electromechanical loading-back system most of elements of the given energy scheme will be absent.

The coefficient of energy efficiency $k_{эфс}$ will be determined by the efficiency of the sources of ES, ES', MS, MS', converters EPC, MPC, and by the energy efficiency coefficients of power transformations in the conventional parts E' and G'.

The energy efficiency coefficient of transformation of electric power $P'_{из}$ into mechanical one P'_d in the engine E' can be represented as [2]

$$\eta_{np1} = \frac{P'_d}{P'_{из}}$$

or

$$\eta_{np1} = 1 - \frac{\Delta P'_d}{P'_{из}}.$$

The energy efficiency coefficient of mechanical power $P'_{им}$ transformation into electrical one P'_r in the generator G' can be represented as [1]

$$\eta_{np2} = \frac{P'_r}{P'_{им}}$$

or

$$\eta_{np2} = 1 - \frac{\Delta P'_r}{P'_{им}}.$$

It should be noted that the additional losses $\Delta P'_d$ and $\Delta P'_r$ are connected with energy process parameters in the main loop, i.e. they are dependent on P_d and P_r correspondingly. Also note that in almost all variants of loading-back systems at least one of the indirect compensation methods of at least one of the loss types in the tested electric machines is used [9].

Coefficients η_{np1} and η_{np2} together with efficiency of all power sources and converters determine the total energy efficiency of loading-back system $k_{эфс}$.

Originality and practical value

It was introduced the concept and proposed the method of analytical determination of the energy efficiency of the loading-back system of traction electric machines. It differs by considering the efficiency of power sources and converters, as well as energy efficiency coefficient of indirect methods to cover losses.

The proposed evaluation methodology of energy efficiency of loading-back system can be used to solve the choice problem of rational circuit design of stands for acceptance testing of electric traction machines of mainline and industrial vehicles.

Conclusions

Energy efficiency of loading-back system is determined by efficiency of power sources and converters, as well as the energy efficiency of indirect methods of loss cover. The losses depend on the share of particular type of loss in the total power loss in the tested electric traction machine.

Reduction of electric energy consumption for electric traction machines testing can be achieved by means of both the choice of rational loading modes [6], and the optimization of the structure of loading-back system.

Minimization of total energy consumption for testing of electric traction machines can be achieved by reducing the number of successive power transformations in auxiliary devices or refusal from such transformations. The most rational seems to be a solution to cover all the losses by a single source of energy. This can be a source of both electrical and mechanical power [9]

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ОПРЕДЕЛЕНИЕ ЭНЕРГЕТИЧЕСКОЙ ЭФФЕКТИВНОСТИ СИСТЕМЫ ВЗАИМНОГО НАГРУЖЕНИЯ ТЯГОВЫХ ЭЛЕКТРИЧЕСКИХ МАШИН

Цель. Приёмо-сдаточные послеремонтные испытания тяговых электромашин проводятся на стендах взаимной нагрузки, которые позволяют снизить общие затраты электроэнергии на испытания. В настоящее время известен целый ряд возможных схемных решений систем взаимного нагружения электромашин, однако отсутствует методика определения их энергетической эффективности. Это, в свою очередь, затрудняет выбор рациональных вариантов. Целью работы является разработка подходящей методики, которая упростит соответствующий процесс. **Методика.** Выражения для определения энергетической эффективности стенда для испытания тяговых электромашин получены путем анализа обобщенной схемы энергетических преобразований в системе взаимного нагружения универсальной структуры. **Результаты.** Предложена методика и получены аналитические выражения для определения энергетической эффективности системы взаимного нагружения тяговых электромашин. Коэффициент энергетической эффективности системы взаимного нагружения предложено рассматривать как отношение общей энергии действия механических и электродвижущих сил, обеспечивающих вращение якорей и протекание токов в испытуемых электромашинах, к суммарной энергии, потребленной за время испытания из внешней сети. **Научная новизна.** Введено понятие и предложен метод аналитического определения энергетической эффективности системы взаимного нагружения тяговых электрических машин, отличающийся учётом в нем к. п. д. источников и преобразователей мощности, а также коэффициентов энергетической эффективности косвенных методов ком-

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пенсации потерь. **Практическая значимость.** Предложенная методика оценки энергетической эффективности системы взаимного нагружения может быть использована при решении задачи выбора рациональных вариантов схемных решений стенов для проведения приёмо-сдаточных испытаний тяговых электромашин магистрального и промышленного транспорта.

Ключевые слова: тяговые электромашини; испытания; взаимная нагрузка; потери мощности; энергетическая эффективность

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ВИЗНАЧЕННЯ ЕНЕРГЕТИЧНОЇ ЕФЕКТИВНОСТІ СИСТЕМИ ВЗАЄМНОГО НАВАНТАЖЕННЯ ТЯГОВИХ ЕЛЕКТРИЧНИХ МАШИН

Мета. Приймально-здавальні післяремонтні випробування тягових електромашин проводяться на стендах взаємного навантаження, які дозволяють знизити загальні витрати електроенергії на випробування. Сьогодні відомий цілий ряд можливих схемних рішень систем взаємного навантаження електромашин, проте відсутня методика визначення їх енергетичної ефективності. Це, в свою чергу, ускладнює вибір раціональних варіантів. Метою роботи є розробка підходящої методики, яка спростить відповідний процес. **Методика.** Вирази для визначення енергетичної ефективності стенов для випробування тягових електромашин отримано шляхом аналізу узагальненої схеми енергетичних перетворень у системі взаємного навантаження універсальної структури. **Результати.** Запропоновано методику й отримано аналітичні вирази для визначення енергетичної ефективності системи взаємного навантаження тягових електромашин. Коефіцієнт енергетичної ефективності системи взаємного навантаження рекомендовано розглядати як відношення загальної енергії дії механічних та електрорушійних сил, що забезпечують обертання якорів і протікання струмів у випробовуваних електромашинах, до сумарної енергії, спожитої за час випробування із зовнішньої мережі. **Наукова новизна.** Введено поняття й запропоновано метод аналітичного визначення енергетичної ефективності системи взаємного навантаження тягових електричних машин, який відрізняється урахуванням у ньому к. к. д. джерел і перетворювачів потужності, а також коефіцієнтів енергетичної ефективності непрямих методів компенсації втрат. **Практична значимість.** Запропонована методика оцінки енергетичної ефективності системи взаємного навантаження може бути використана при вирішенні задач вибору раціональних варіантів схемних рішень стенов для проведення приймально-здавальних випробувань тягових електромашин магистрального й промислового транспорту.

Ключові слова: тягові електромашини; випробування; взаємне навантаження; втрати потужності; енергетична ефективність

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